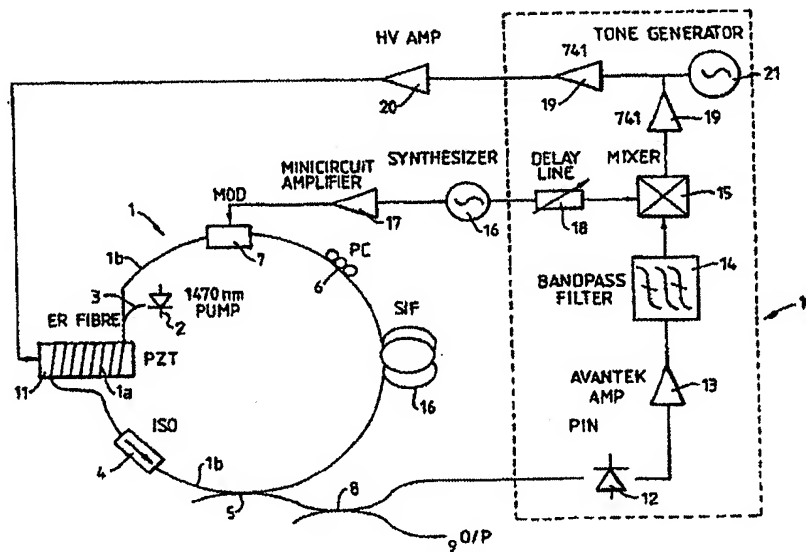


## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 5 : H01S 3/098, 3/06, 3/139	A1	(11) International Publication Number: <b>WO 94/19847</b> (43) International Publication Date: 1 September 1994 (01.09.94)
(21) International Application Number: PCT/GB94/00355 (22) International Filing Date: 23 February 1994 (23.02.94) (30) Priority Data: 93301413.6 25 February 1993 (25.02.93) EP (34) Countries for which the regional or international application was filed: AT et al. (71) Applicant (for all designated States except US): BRITISH TELECOMMUNICATIONS PUBLIC LIMITED COMPANY [GB/GB]; 81 Newgate Street, London EC1A 7AJ (GB). (72) Inventor; and (75) Inventor/Applicant (for US only): SHAN, Xuekang [CN/GB]; 99 Rushmere Road, Ipswich, Suffolk IP4 4LQ (GB). (74) Agent: PRATT, David, Martin; BT Group Legal Services, Intellectual Property Dept., 13th floor, 151 Gower Street, London WC1E 6BA (GB).		(81) Designated States: AU, CA, CN, GB, JP, NZ, US, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published With international search report.

## (54) Title: MODE-LOCKED FIBRE RING LASER STABILISATION



## (57) Abstract

A method is described of stabilising the output of a mode-locked fibre ring laser (1). The fibre constituting the laser (1) includes a dopant in its core. The method comprises the steps of adjusting the length of the ring laser (1) to minimise variations in its cavity length, and hence lock the phase of the laser output pulses with that of its drive source (2), and subjecting a portion (1a) of the fibre of the ring laser (1) to vibrations at a predetermined frequency whose period is less than the dopant ion upper state lifetime.

**FOR THE PURPOSES OF INFORMATION ONLY**

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

AT	Austria	GB	United Kingdom	MR	Mauritania
AU	Australia	GE	Georgia	MW	Malawi
BB	Barbados	GN	Guinea	NE	Niger
BE	Belgium	GR	Greece	NL	Netherlands
BF	Burkina Faso	HU	Hungary	NO	Norway
BG	Bulgaria	IE	Ireland	NZ	New Zealand
BJ	Benin	IT	Italy	PL	Poland
BR	Brazil	JP	Japan	PT	Portugal
BY	Belarus	KE	Kenya	RO	Romania
CA	Canada	KG	Kyrgyzstan	RU	Russian Federation
CF	Central African Republic	KP	Democratic People's Republic of Korea	SD	Sudan
CG	Congo	KR	Republic of Korea	SE	Sweden
CH	Switzerland	KZ	Kazakhstan	SI	Slovenia
CI	Côte d'Ivoire	LI	Liechtenstein	SK	Slovakia
CM	Cameroon	LK	Sri Lanka	SN	Senegal
CN	China	LU	Luxembourg	TD	Chad
CS	Czechoslovakia	LV	Latvia	TG	Togo
CZ	Czech Republic	MC	Monaco	TJ	Tajikistan
DE	Germany	MD	Republic of Moldova	TT	Trinidad and Tobago
DK	Denmark	MG	Madagascar	UA	Ukraine
ES	Spain	ML	Mali	US	United States of America
FI	Finland	MN	Mongolia	UZ	Uzbekistan
FR	France			VN	Viet Nam
GA	Gabon				

MODE-LOCKED FIBRE RING LASER STABILISATION

This invention relates to a method of, and apparatus for, stabilising the output of a mode-locked fibre ring laser, and to a mode-locked fibre ring laser.

5 Mode-locked fibre ring lasers offer potentially the best quality (pulse width, pulse shape and time x bandwidth) optical source for producing solitons. A fibre laser typically needs to contain tens or even hundreds of metres of fibre for two reasons: to obtain sufficient gain from the  
10 rare-earth-doped fibre, and also to include all required intra-cavity components to enable controlled operation. The fundamental frequency of a laser cavity of this length is in the MHz region. Hence, to use a fibre laser as a source of optical pulses at GHz frequencies (the range of most interest  
15 to communications systems at present), it is necessary to achieve stable operation at very high harmonics of the fundamental cavity frequency. This requires active control of the length of the fibre laser. Mode-locking at high harmonics, and the susceptibility of fibre to its  
20 environment, lead to output noise and instability, unless unwanted cavity modes can be suppressed and the cavity length kept at the right value. Harmonically mode-locked lasers behave quite differently from fundamentally mode-locked lasers; and, generally speaking, their output is inherently  
25 noisier. This is due to supermode competitions associated with harmonic mode-locking. The reasons for this will now be explained.

Thus, in an Nth harmonic mode-locked laser, the cavity mode spacing is  $f_c$ , and the modulation frequency  $f_m = Nf_c$ . An  
30 axial mode is not locked to its nearest neighbours, but to the ones N axial modes apart on each side. All the modes within the linewidth are thus grouped into N sets, or into N so-called supermodes. Every supermode forms a separate mode-locking solution, and satisfies all the modulation and lasing  
35 conditions. As a result, all these modes can oscillate at the same time more or less independently and compete against

each other, unless one of them, for some reason, saturates the gain and thus suppresses the others. The energy shift among these supermodes, and the relative phase slides between them, readily leads to pulse amplitude fluctuations and even  
5 to missing of some pulses. Reflections (e.g. from intra-cavity elements) into the gain medium (erbium fibre in this case) affects the mode competition, as they form standing waves in the lasing medium, and thus cause spatial hole burning. In simple erbium fibre ring laser operations,  
10 sporadic noise bursts, which are related to supermode beatings in the laser's radio frequency (RF) spectrum, are observed. Letting only one supermode oscillate is the key to the stable operation of such lasers.

An effective way to suppress the unwanted supermodes  
15 is (see "Harmonically mode-locked fiber ring laser with an internal Fabry-Perot stabilizer for soliton transmission" - Optics Letters, vol. 18, No. 2, January 1993) to insert a high finesse Fabry-Perot etalon into the fibre cavity, the etalon having a free spectral range which is exactly equal to  
20 the pulse repetition rate. The etalon acts as a very narrow band-pass comb filter, and so picks up only one supermode. The intra-cavity etalon needs careful control, and a separate cavity length adjustment is still required.

The present invention provides a method of stabilising  
25 the output of a mode-locked fibre ring laser, the fibre constituting the laser including a dopant in its core, the method comprising the steps of adjusting the length of the ring laser to minimise variations in its cavity length, and hence lock the phase of the laser output pulses with that of  
30 its drive source, and subjecting a portion of the fibre of the ring laser to vibrations at a predetermined frequency whose period is less than the dopant ion upper state lifetime.

Advantageously, the length of the ring laser is  
35 adjusted by means of a piezoelectric device, the ring laser is mode-locked by a modulator driven by a synthesizer, and the piezoelectric device is driven by a feedback circuit

which compares the phase of the laser output signal with the phase of the synthesizer and outputs an error signal which drives the piezoelectric device to minimise the deviation of the phase of the laser output from its desired value.

5 Preferably, a frequency mixer is used to compare the phase of the laser output signal and the phase of the synthesizer, and a tone generator is included in the feedback circuit between the mixer and the piezoelectric device, the tone generator being effective to subject said fibre portion  
10 to vibrations at said predetermined frequency. The tone generator may superimpose a tone of a second predetermined frequency into the feedback circuit, the second predetermined frequency being such that the first-mentioned predetermined frequency is equal to, or a harmonic of, the second  
15 predetermined frequency.

The invention also provides apparatus for stabilising the output of a mode-locked fibre ring laser, the fibre constituting the laser including a dopant in its core, the apparatus comprising means for adjusting the length of the  
20 ring laser to minimise variations in its cavity length, and hence lock the phase of the laser output pulses with that of its drive source, and means for subjecting a portion of the fibre of the ring laser to vibrations at a predetermined frequency whose period is less than the dopant ion upper  
25 state lifetime.

Advantageously, a piezoelectric device constitutes the means for adjusting the length of the ring laser, and the apparatus further comprises a modulator and a synthesizer, the synthesizer driving the modulator to mode-lock the ring  
30 laser.

Preferably, the apparatus further comprises a feedback circuit for driving the piezoelectric device to adjust the length of the ring laser, the feedback circuit comparing the phase of the laser output signal with the phase of the  
35 synthesizer and outputting an error signal which drives the piezoelectric device to minimise the deviation of the phase of the laser output from its desired value. Conveniently,

the feedback circuit includes a frequency mixer for comparing the phase of the laser output signal and the phase of the synthesizer.

In a preferred embodiment, the apparatus further  
5 comprises a tone generator for superimposing a signal of a second predetermined frequency into the feedback circuit downstream of the mixer, the tone generator constituting the means for subjecting said fibre portion to vibrations at said predetermined frequency. Advantageously, the tone generator  
10 is such that the first-mentioned predetermined frequency is equal to, or harmonic of, the second predetermined frequency.

The invention further provides a mode-locked fibre ring laser comprising a fibre ring laser, an optical pump source for driving the ring laser, means for mode-locking the  
15 output of the ring laser, and apparatus for stabilising the output of the ring laser, the fibre constituting the ring laser including a dopant in its core, the mode-locking means being constituted by a modulator positioned within the ring laser, and the modulator being driven by a synthesizer,  
20 wherein means are provided for adjusting the length of the ring laser to minimise variations in its cavity length, and hence lock the phase of the laser output pulses with that of the drive source, and wherein the stabilising apparatus is as defined above.

25 Preferably, a laser diode constitutes the optical pump source.

The invention will now be described in greater detail, by way of example, with reference to the accompanying drawings, in which: -

30 Figure 1 is a circuit diagram of the mode-locked fibre ring laser stabilisation scheme of the invention;

Figure 2a to 2d are RF spectra of the laser mode-locked at 2.5GHz and illustrate the stabilising effect of the scheme of Figure 1 on the laser output; and

35 Figure 3 compares an optical pulse (as observed with a fast pin/sampling scope) from the laser when utilising the scheme of Figure 1 and when not utilising that scheme.

Referring to the drawings, Figure 1 shows a fibre ring laser 1 constituted by 30m of erbium fibre 1a and 70m of step index fibre (SIF) 1b having a dispersion of 16ps/nm/km at 1560nm. The total cavity length of the laser 1 is, therefore, 100m; and this corresponds to a cavity mode spacing of about 2MHz. The SIF 1b ensures that the peak optical power of the laser 1 is close to the fundamental soliton power in the fibre, resulting in more stable operation.

The fibre ring laser 1 is pumped by a 1470nm laser diode 2 via a coupler 3. An isolator 4 is provided in the ring laser 1 between the erbium fibre 1a and an output coupler 5, to minimise the effect of reflection from the output end and ensure unidirectional operation. If the laser 1 was allowed to work in both directions, its output would tend to incorporate instabilities. A polarisation controller 6 is also provided in the ring laser 1. The output of the laser is mode locked by means of an electro-optic (a lithium niobate) phase modulator 7 having an insertion loss of ~6dB and a 3dB bandwidth of ~2.5GHz. The modulator 7 is, therefore, effective to mode-lock the laser 1 at ~2.5GHz, which is about the 1250th harmonic of the fundamental cavity frequency. The polarisation controller 6 is required as the modulator 7 is polarisation sensitive.

The output coupler 5 is a 50/50 coupler, this coupler leading to the laser output 8 via a further coupler 9. The coupler 9 is a 90/10 coupler, with 90% of its input leading to the laser output 8, and 10% leading to a stability circuit indicated generally by the reference numeral 10. Stabilisation of the output of the laser 1 is necessary, because of its susceptibility to mechanical vibrations and temperature variations which affect its cavity length, and hence the mode-locking process. Stabilisation is affected by a piezoelectric drum 11 which is driven by the circuit 10 so as to maintain the cavity length of the laser 1 substantially constant. The erbium fibre 1a is wound around the drum 11.

The stabilising circuit 10 includes a PIN diode 12 (a

BT&D 20GHz PIN diode) which converts the optical signal input thereto into an electrical output signal. This electrical signal is amplified by an Avantek 6GHz, 20dB gain amplifier 13, and is then passed to a Watkins Johnson M15C frequency mixer 15 via a Declan BA 2488-50 bandpass filter 14 (this filter having a pass band of 50 MHz centred on a frequency of 2.488 GHz).

The modulator 7 is driven by a synthesizer 16 via an RF amplifier 17. The synthesizer 16 is an HP83620A device, and the RF amplifier 17 is a Minicircuit Laboratories ZHL-1042J. The output of the synthesizer 16 is also passed to the mixer 15, via a delay line 18. The mixer 15 compares the phase  $\theta_p(t)$  of the laser output pulse with the phase  $\theta_s$  the synthesizer output, and outputs an error signal  $u(t)$ , where: -

$$u(t) = Ky_s y_p(t) \cos [\theta_s - \theta_p(t) + \Psi]$$

when  $y_s$  and  $y_p(t)$  are the inputs to the mixer from the synthesizer 16 and the laser 1 respectively,  $K$  is the conversion constant of the mixer, and  $\Psi$  is introduced by the adjustable delay line 18. The length of the delay line 18 is adjusted to ensure that the two signals input into the mixer 15 are in phase, that is to say

$$\theta_s + \Psi = \pi/2$$

When the pulse is best,  $\theta_p(t) \sim 0$  and the mixer output then is: -

$$u(t) = Ky_s y_p(t) \sin \theta_p(t)$$

which is clearly a good error signal for small deviations of  $\theta_p(t)$ .

The output of the mixer 15 is fed, via two 741 op-amps 19 and a high voltage amplifier 20 to the piezoelectric drum 11, thus forming a negative feedback loop which is effective to displace the drum to adjust the length of the fibre ring to keep the deviation  $\theta_p(t)$  at a minimum value. In this way, the fibre cavity length is maintained at the desired level, and optical pulses can last for hours in contrast to only the few minutes that are possible without the feedback.

The stabilisation circuit 10 as described above is known (see "Stabilising Er Fibre Soliton Laser With Pulse



Phase Locking" - Electronics Letters 16 January 1992, Vol. 28 No. 2 pages 182-183). Unfortunately, as explained above, unwanted cavity mode beatings (caused by supermode competition) occur. These unwanted beatings (see Figures 2a and 2b) are spaced 2MHz apart and overlay the desired beatings which are ~ 2.5 GHz apart. They contribute to the pulsed optical output of the laser 1 simply as noise.

In order to suppress the sporadic bursts caused by these unwanted beatings, the known stabilisation circuit is modified by the inclusion of a tone generator 21. The tone generator produces a signal of ~ 14KHz, which is mixed with the error signal output by the mixer 15 downstream of the first op-amp 19. As shown in Figures 2c and 2d, the effect of the tone signal is to remove substantially all the noise by suppressing the supermode beatings (the 2MHz components) by more than 10dB (optical power), so that the dominant supermode is more than 25dB higher than the unwanted supermodes. In this connection, Figure 2c should be compared with Figure 2a and Figure 2d should be compared with Figure 2b; from which it will be noted that, when the tone is not present, the dominant supermode is only 15 to 20dB higher than the unwanted supermodes. Figure 3 illustrates the improvement which results from using the known stabilisation circuit with (see Figure 3a) and without (see Figure 3b) the tone. As will be apparent, when the tone is present, the optical pulse output by the ring laser 1 is much cleaner.

The optimum tone frequency for the laser 1 described above (that is to say one which is mode-locked at ~ 2.5GHz) has been found empirically to be ~ 14kHz, which corresponds to a mechanical resonance of the piezoelectric drum 11 used, the drum actually vibrating at 28kHz (the second harmonic of the optimum tone frequency). With the tone optimised, the laser 1 generates pulses with ~ 20 ps full width half maximum (FWHM) at ~ 2.5GHz, the time-bandwidth product is ~ 0.4, and the pulse-to-pulse timing jitter is ~ 1 ps as measured with an HP digitising scope. Soliton data can be transmitted over 205km fibre, using this laser as the source, with not a

single error being detected within 100 minutes, given a BER better than  $10^{-13}$ . It is also possible to transmit solitons generated by this laser in a recirculating loop, and to achieve a  $10^{-9}$  bit error rate at 12,000 km, this being the  
5 limit imposed by Gordon-Haus jitter. In either case, when the tone is switched off (or its frequency is tuned away from the resonance), the transmissions suffer from sporadic noise bursts, and long term (minutes) error-free operation is impossible.

10       How the tone leaves only one supermode oscillating and suppresses the others is not fully understood, though it is believed that, when several supermodes are present, there is a standing wave pattern in the gain medium caused by weak reflections in the ring cavity due to the presence of the  
15 modulator 7 and the isolator 4. This standing wave pattern causes spatial hole burning which reduces cross-mode saturation and so affects mode competition. As a result, it is difficult for any one supermode to saturate the gain, and more supermodes are likely to be present. The tone, however,  
20 shakes (dithers) the erbium fibre at a rate (frequency) whose period is much less than the erbium ion upper state lifetime ( $\sim 10$ ms), thus preventing the standing wave pattern from being formed, and thereby washing out spatial hole burning (but there are still reflections). The faster the shake compared  
25 to the erbium life time, the more effective the suppression. The fastest possible rate for the particular HV amp/PZT combination is  $\sim 28$  kHz.

CLAIMS

1. A method of stabilising the output of a mode-locked fibre ring laser, the fibre constituting the laser including a dopant in its core, the method comprising the steps of  
5 adjusting the length of the ring laser to minimise variations in its cavity length, and hence lock the phase of the laser output pulses with that of its drive source, and subjecting a portion of the fibre of the ring laser to vibrations at a predetermined frequency whose period is less than the dopant  
10 ion upper state lifetime.
2. A method as claimed in claim 1, wherein the length of the ring laser is adjusted by means of a piezoelectric device.
3. A method as claimed in claim 2, wherein the ring laser  
15 is mode-locked by a modulator driven by a synthesizer, and wherein the piezoelectric device is driven by a feedback circuit which compares the phase of the laser output signal with the phase of the synthesizer and outputs an error signal which drives the piezoelectric device to minimise the  
20 deviation of the phase of the laser output from its desired value.
4. A method as claimed in claim 3, in which a frequency mixer is used to compare the phase of the laser output signal and the phase of the synthesizer, and a tone generator is  
25 included in the feedback circuit between the mixer and the piezoelectric device, the tone generator being effective to subject said fibre portion to vibrations at said predetermined frequency.
5. A method as claimed in claim 4, in which the tone  
30 generator superimposes a tone of a second predetermined frequency into the feedback circuit, the second predetermined frequency being such that the first-mentioned predetermined

frequency is equal to, or a harmonic of, the second predetermined frequency.

6. Apparatus for stabilising the output of a mode-locked fibre ring laser, the fibre constituting the laser including  
5 a dopant in its core, the apparatus comprising means for adjusting the length of the ring laser to minimise variations in its cavity length, and hence lock the phase of the laser output pulses with that of its drive source, and means for  
10 subjecting a portion of the fibre of the ring laser to vibrations at a predetermined frequency whose period is less than the dopant ion upper state lifetime.

7. Apparatus as claimed in claim 6, wherein a piezoelectric device constitutes the means for adjusting the length of the ring laser.

15 8. Apparatus as claimed in claim 7, further comprising a modulator and a synthesizer, the synthesizer driving the modulator to mode-lock the ring laser.

9. Apparatus as claimed in claim 8, further comprising a  
20 feedback circuit for driving the piezoelectric device to adjust the length of the ring laser, the feedback circuit comparing the phase of the laser output signal with the phase of the synthesizer and outputting an error signal which drives the piezoelectric device to minimise the deviation of the phase of the laser output from its desired value.

25 10. Apparatus as claimed in claim 9, wherein the feedback circuit includes a frequency mixer for comparing the phase of the laser output signal and the phase of the synthesizer.

11. Apparatus as claimed in claim 10, further comprising  
30 a tone generator for superimposing a signal of a second predetermined frequency into the feedback circuit downstream of the mixer, the tone generator constituting the means for

subjecting said fibre portion to vibrations at said predetermined frequency.

12. Apparatus as claimed in claim 11, wherein the tone generator is such that the first-mentioned predetermined frequency is equal to, or harmonic of, the second predetermined frequency.

13. A mode-locked fibre ring laser comprising a fibre ring laser, an optical pump source for driving the ring laser, means for mode-locking the output of the ring laser, and apparatus for stabilising the output of the ring laser, the fibre constituting the ring laser including a dopant in its core, the mode-locking means being constituted by a modulator positioned within the ring laser, and the modulator being driven by a synthesizer, wherein means are provided for adjusting the length of the ring laser to minimise variations in its cavity length, and hence lock the phase of the laser output pulses with that of the drive source, and wherein the stabilising apparatus is as claimed in any one of claims 7 to 12.

14. A ring laser as claimed in claim 13, wherein a laser diode constitutes the optical pump source.

3/4

Fig.2c.

RL 2.50 dBm  
ATTEN. 15dB  
5.00 dB/DIV  
AVG. PWR. -1.2dBm  
REFERENCE LEVEL  
2.50 dBm

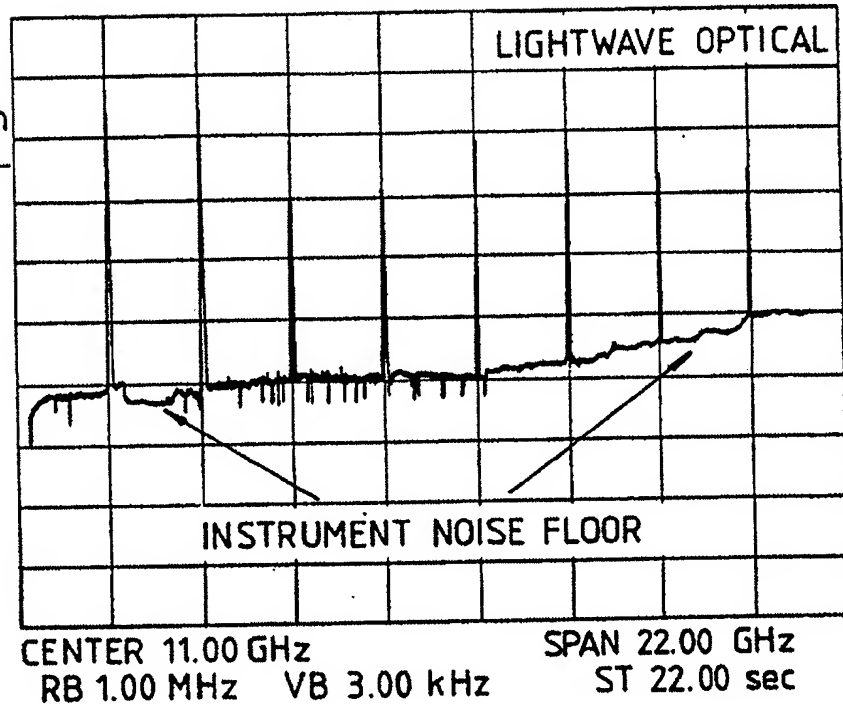
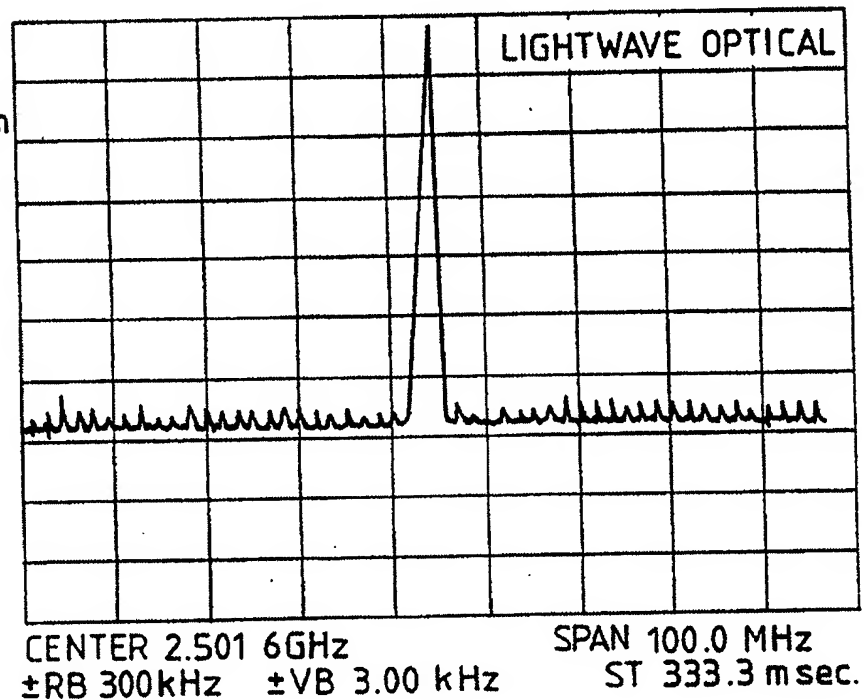


Fig.2d.

RL 2.50 dBm  
ATTEN. 15dB  
5.00 dB/DIV  
AVG. PWR. -1.2dBm  
RES BANDWIDTH  
300 kHz



4/4

Fig. 3a.

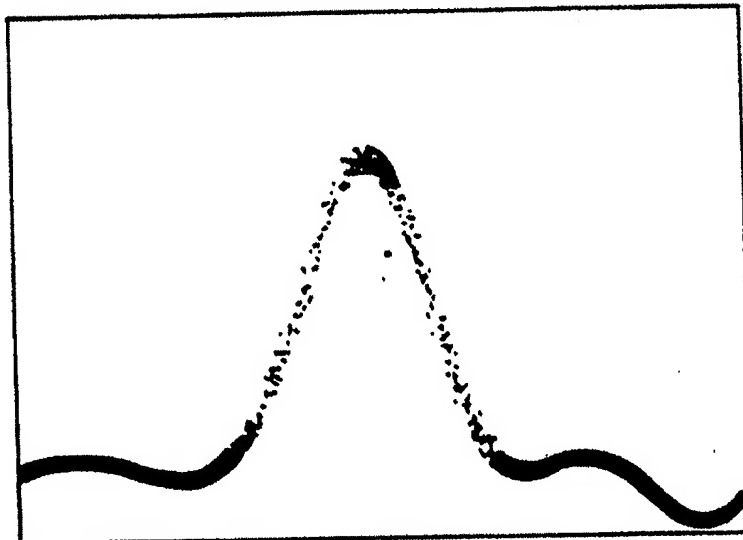
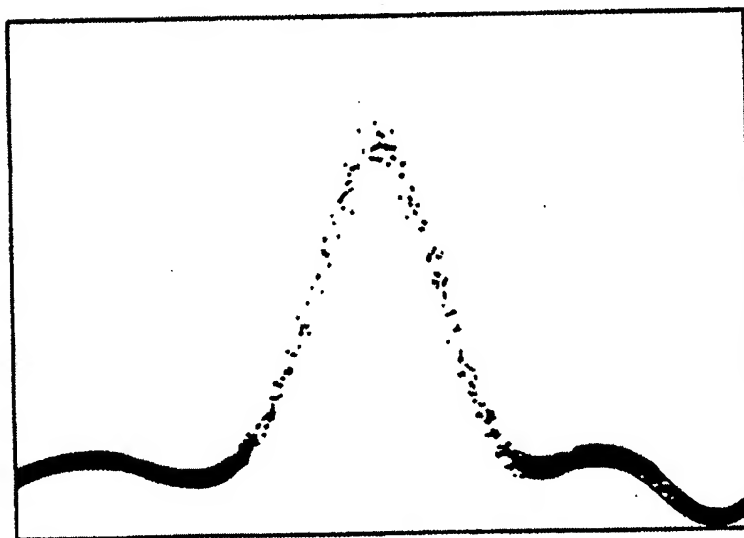


Fig. 3b.



A. CLASSIFICATION OF SUBJECT MATTER  
 IPC 5 H01S3/098 H01S3/06 H01S3/139

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
 IPC 5 H01S

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	ELECTRONICS LETTERS., vol.28, no.2, 16 January 1992, ENAGE GB pages 182 - 184, XP000280611 X.SHAN ET AL. 'Stabilising Er fibre soliton laser with pulse phase locking' cited in the application see the whole document ----	1-14
Y	APPLIED PHYSICS LETTERS., vol.58, no.21, 27 May 1991, NEW YORK US pages 2323 - 2325, XP000238142 H.SABERT ET AL. 'Spatial hole burning in Nd3+ fiber lasers suppressed by push-pull phase modulation' see page 2323, column 1, line 40 - column 2, line 18; figure 1C ----- -/-	1-14

☒ Further documents are listed in the continuation of box C.

☐ Patent family members are listed in annex.

\* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
- "E" earlier document but published on or after the international filing date
- "F" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)
- "O" document referring to an oral disclosure, use, exhibition or other means
- "P" document published prior to the international filing date but later than the priority date claimed

"I" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

- "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

Date of the actual completion of the international search

7 June 1994

Date of mailing of the international search report

15.06.94

Name and mailing address of the ISA

European Patent Office, P.O. 5818 Patentlaan 2  
 NL - 2280 HT Rijswijk  
 Tel. (+31-70) 340-2040, Tx. 31 651 epo nl,  
 Fax (+31-70) 340-3016

Authorized officer

Galanti, M



## C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	<p>OPTICS LETTERS., vol.18, no.2, 15 January 1993, NEW YORK US pages 107 - 109, XP000331296 G.T.HARVEY ET AL. 'Harmonically mode-locked fiber ring laser with an internal Fabry-Perot stabilizer for soliton transmission' cited in the application see abstract</p>	1
A	<p>--- REVIEW OF SCIENTIFIC INSTRUMENTS, vol.60, no.4, April 1989, NEW YORK US pages 592 - 597 H.VANHERZEELE 'Characterization and active stabilization of a harmonically modulated continuous-wave Nd:LiYF<sub>4</sub> laser' see abstract; figure 2</p>	1
A	<p>--- APPLIED PHYSICS LETTERS., vol.16, no.3, 1 February 1970, NEW YORK US pages 124 - 126 H.G.DANIELMEYER ET AL 'Spontaneous single frequency output from a spatially homogeneous Nd:YAG laser' see abstract</p>	1
A	<p>--- APPLIED PHYSICS, vol.3, 1974, HEIDELBERG DE pages 193 - 198 H.G.DANIELMEYER 'Stable tunable single-frequency Nd:YAG laser' see abstract; figure 1</p>	1
P,X	<p>--- ELECTRONICS LETTERS., vol.29, no.11, 27 May 1993, ENAGE GB pages 978 - 981, XP000372912 SHAN X. ET AL. 'Novel method to suppress noise in harmonically modelocked erbium fibre lasers' see the whole document</p>	1-14